



Engineered Wetlands for Treating Petroleum Hydrocarbon- Contaminated Water



Brian Davis, Ph.D.

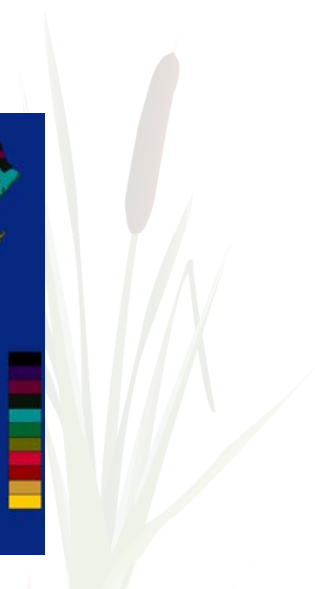
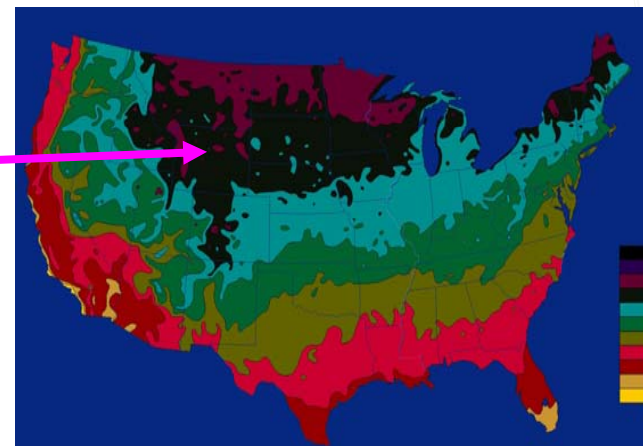
Scott Wallace, PE





Casper Refinery Site

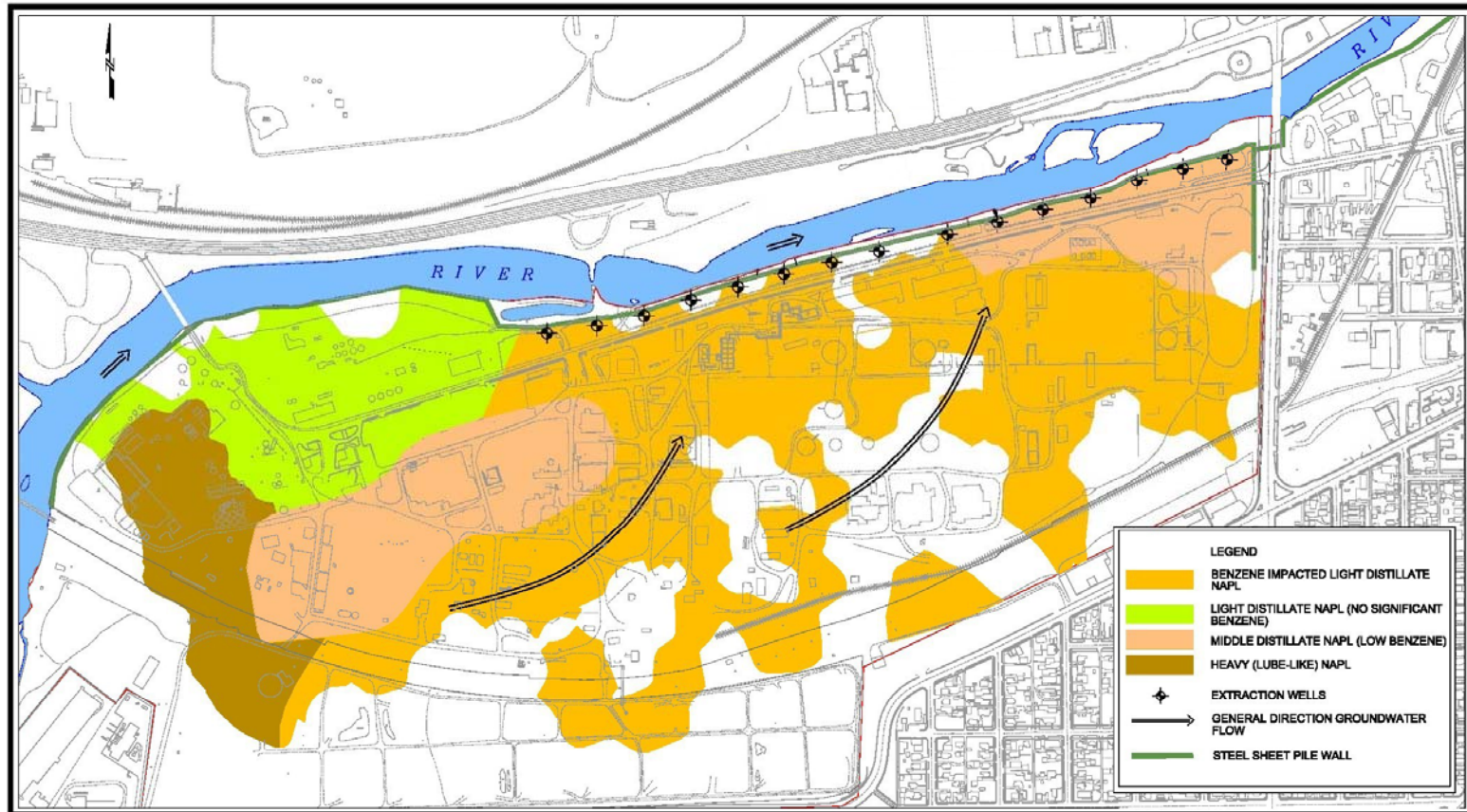
- Operated 1912 to 1991
- 37,000 m³ of LNAPL recovered to date
- Extensive smear zone due to changing water table elevation
- 50 to 100 years to remediate site
- High mountain west: -35°C

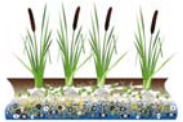




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LNAPL Distribution





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Reuse Plan



SSF Wetlands

FWS Wetlands

PLATTE RIVER COMMONS MASTER PLAN DRAFT
CASPER, WYOMING

MAY 2002



DESIGNWORKSHOP
Landscape Architecture • Land Planning • Urban Design • Interior Planning
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Treatment Needs

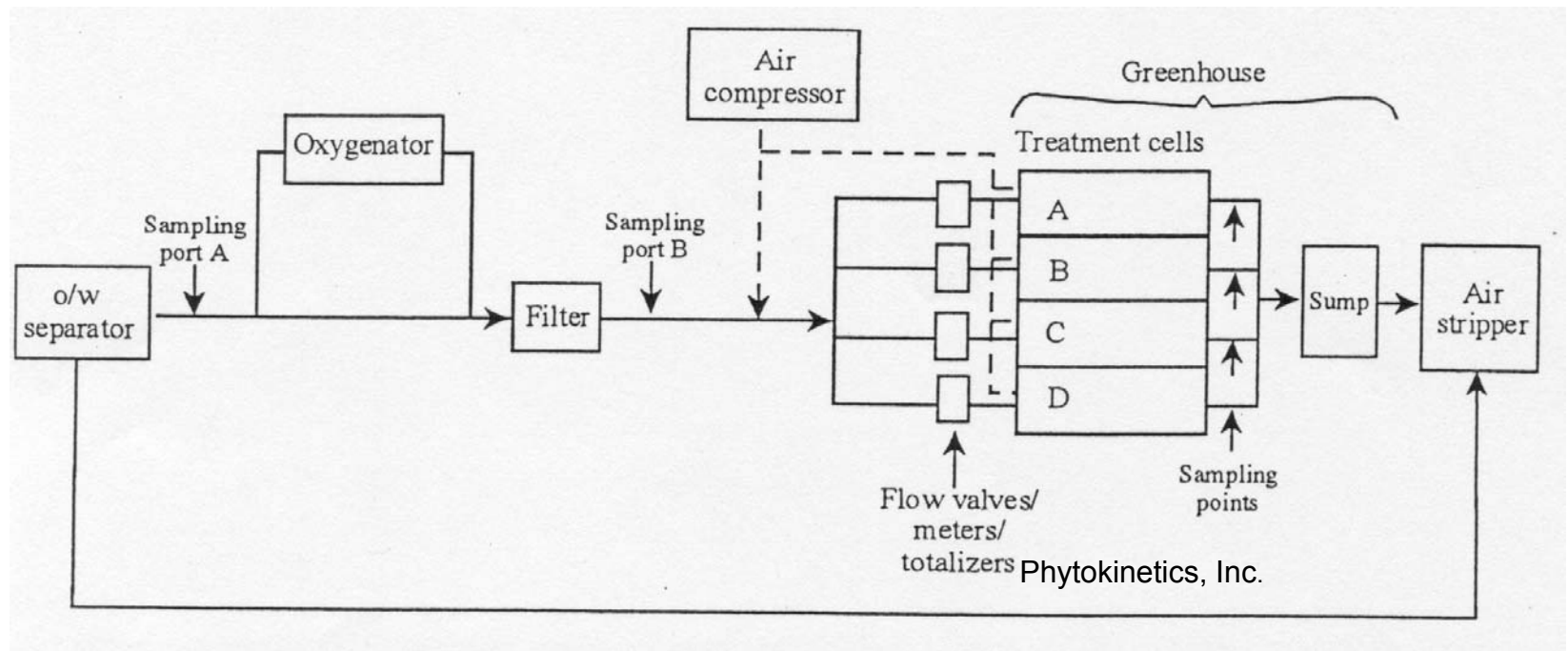
- Influent benzene ~ 1.5 mg/L
- Effluent benzene < 0.5 mg/L due to RCRA requirements
- Final benzene < 0.05 mg/L to meet permit limit
- Final iron < 2 mg/L
- Operate at -35°C
- Pilot system operated to demonstrate concept, develop removal rates





Pilot Wetland System

- 4 cells
- Vertical upward flow
- With and without aeration
- With and without wetland sod

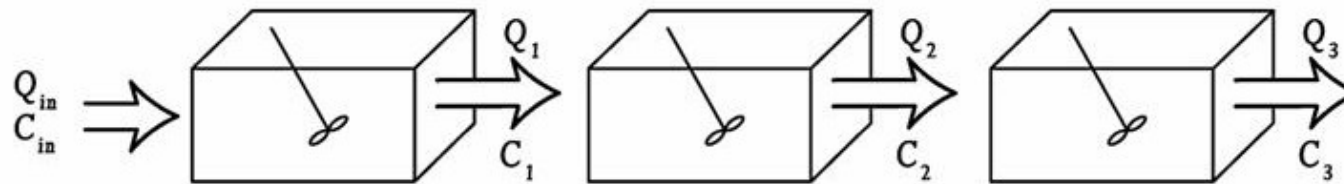




Pilot Unit Results

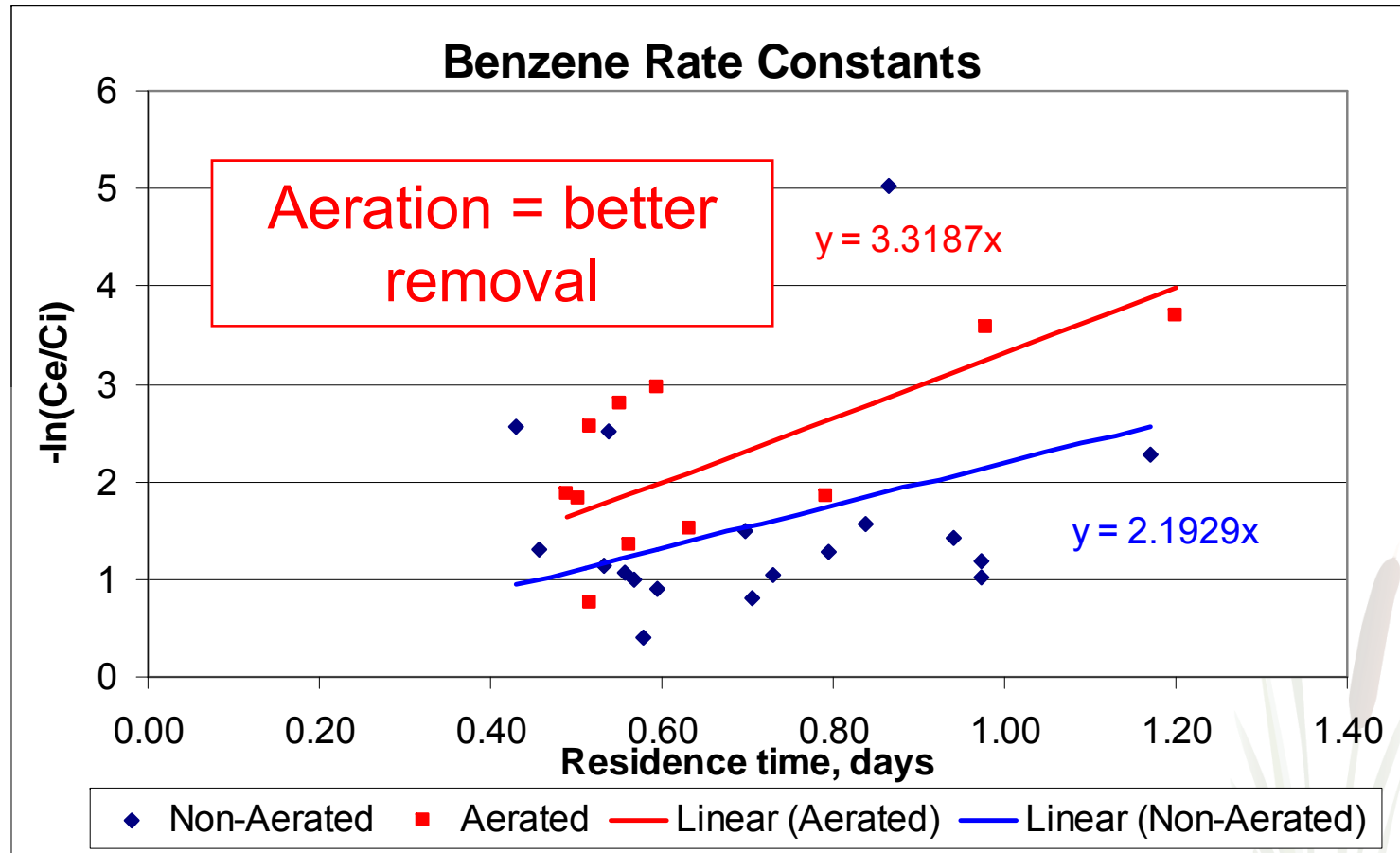
k_A , m/yr, based on 3 TIS

Compound	Aeration		No Aeration	
	Wetland Mulch	No Mulch	Wetland Mulch	No Mulch
Benzene	518	456	317	256
BTEX	356	311	257	244
TPH	1,058	965	725	579
MTBE	64	60	35	22





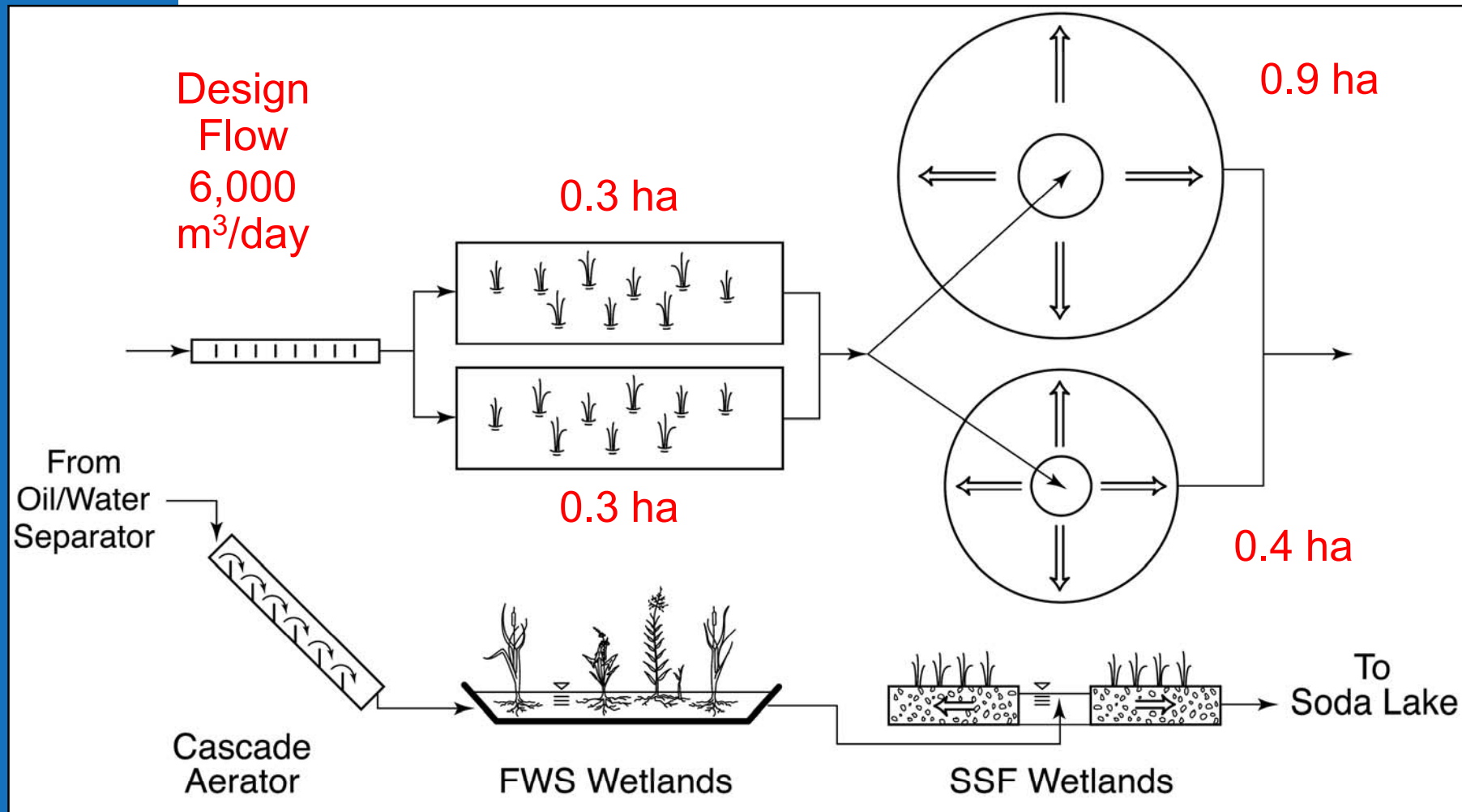
Pilot Results: Aerated vs. Non-aerated



Area: 4 ha → 1.3 ha



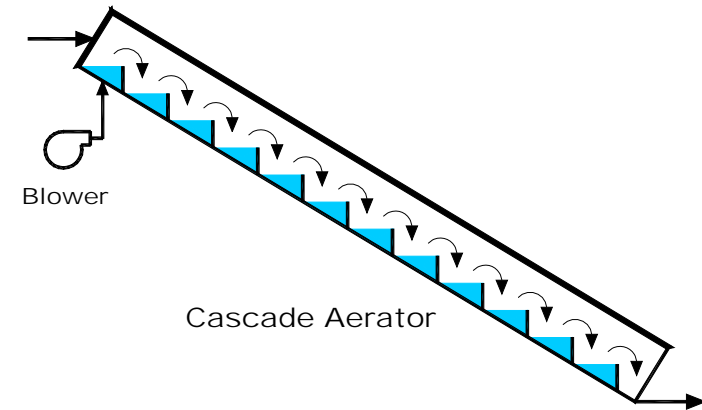
Full Scale System





Cascade Aerator

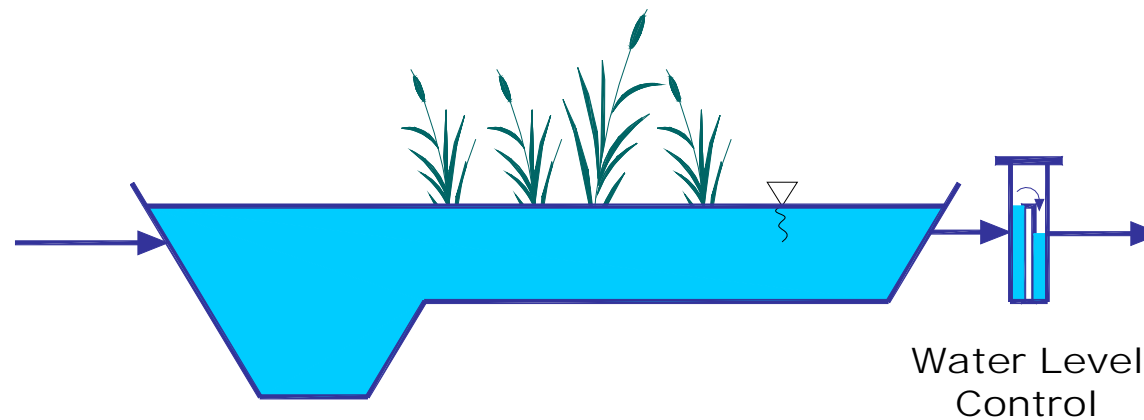
- Oxidize Fe^{2+} to Fe^{3+}
- Benzene air stripping (1.5 → 0.5 mg/l at 3,000 m^3/day)
- Option to add second cascade for total capacity of 6,000 m^3/day





Surface Flow Wetland

- Iron removal by sedimentation
- Deep zones for sludge removal

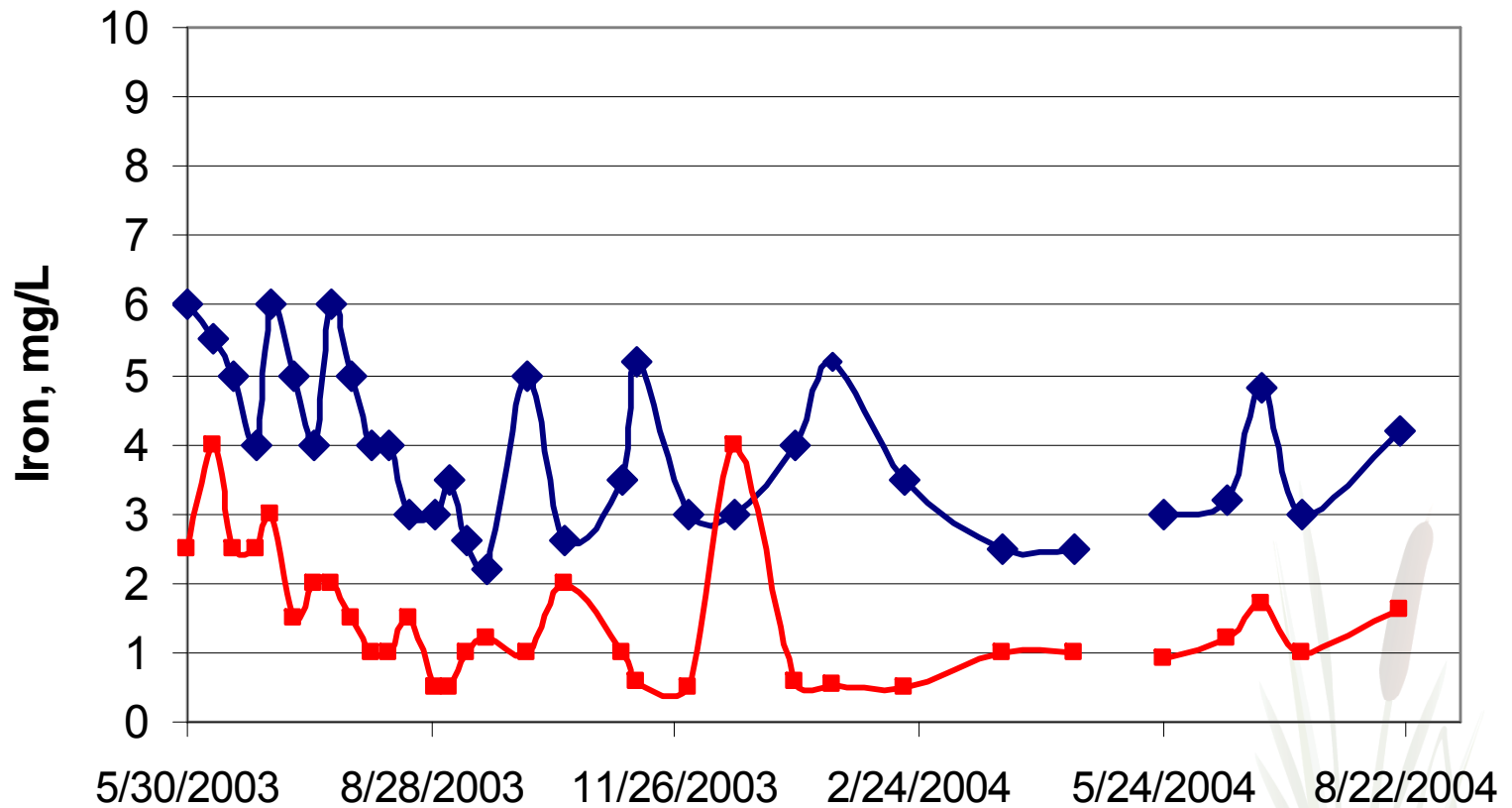


Iron Removal Wetlands





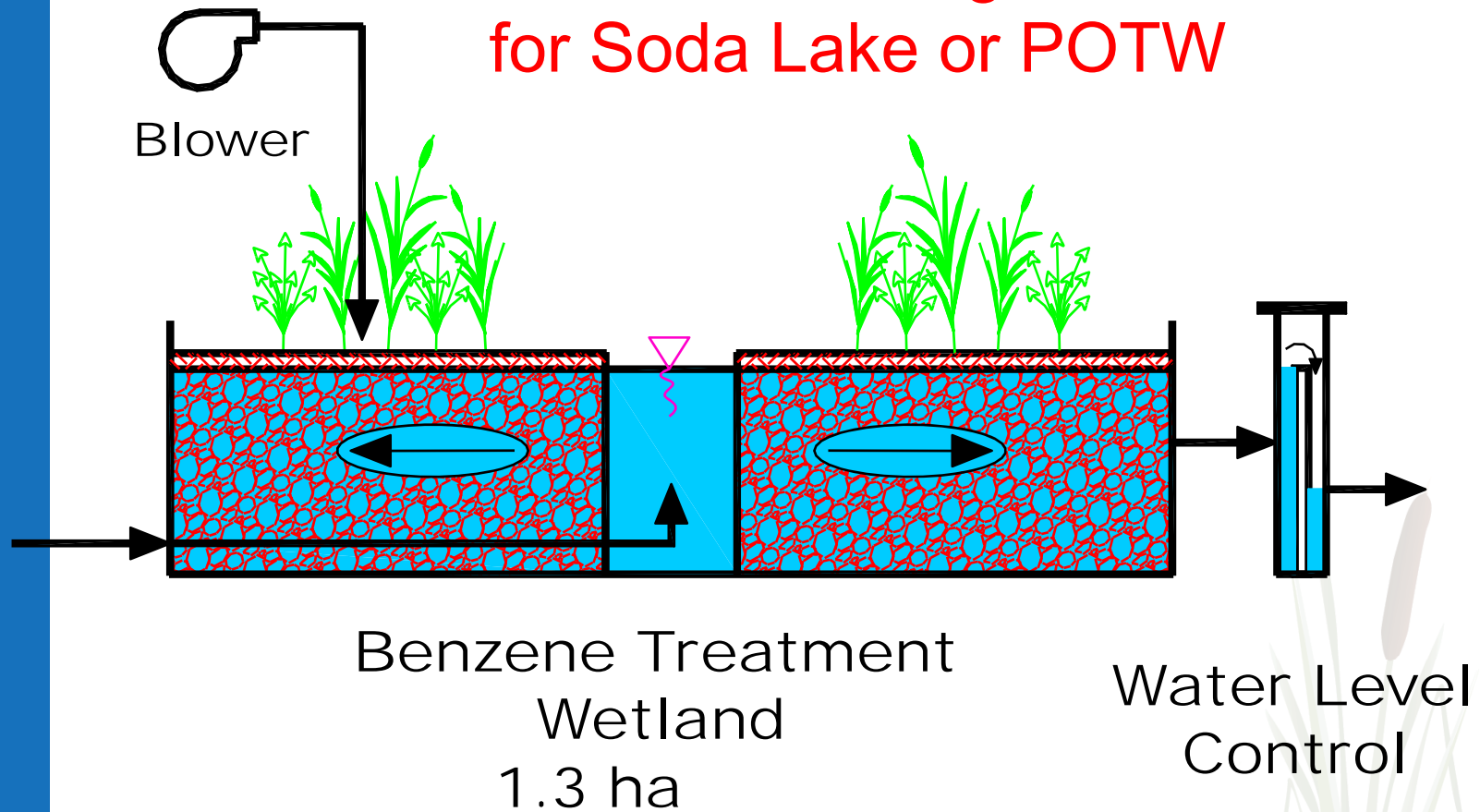
Surface Flow Wetland Iron Removal





Subsurface Flow Wetlands

- Achieve 0.05 mg/L benzene limit for Soda Lake or POTW



- Hydraulically pass 8.3 m³/min



SSF Wetland Air Distribution





SSF Wetland Construction





SSF Wetland Construction

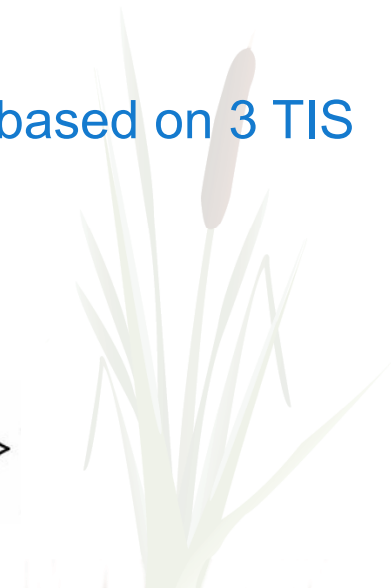
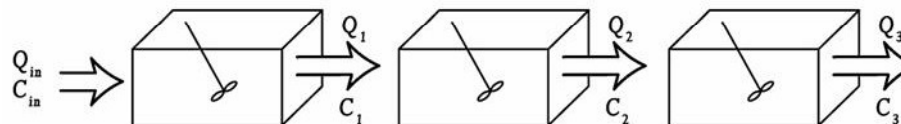




Treatment Wetland Performance

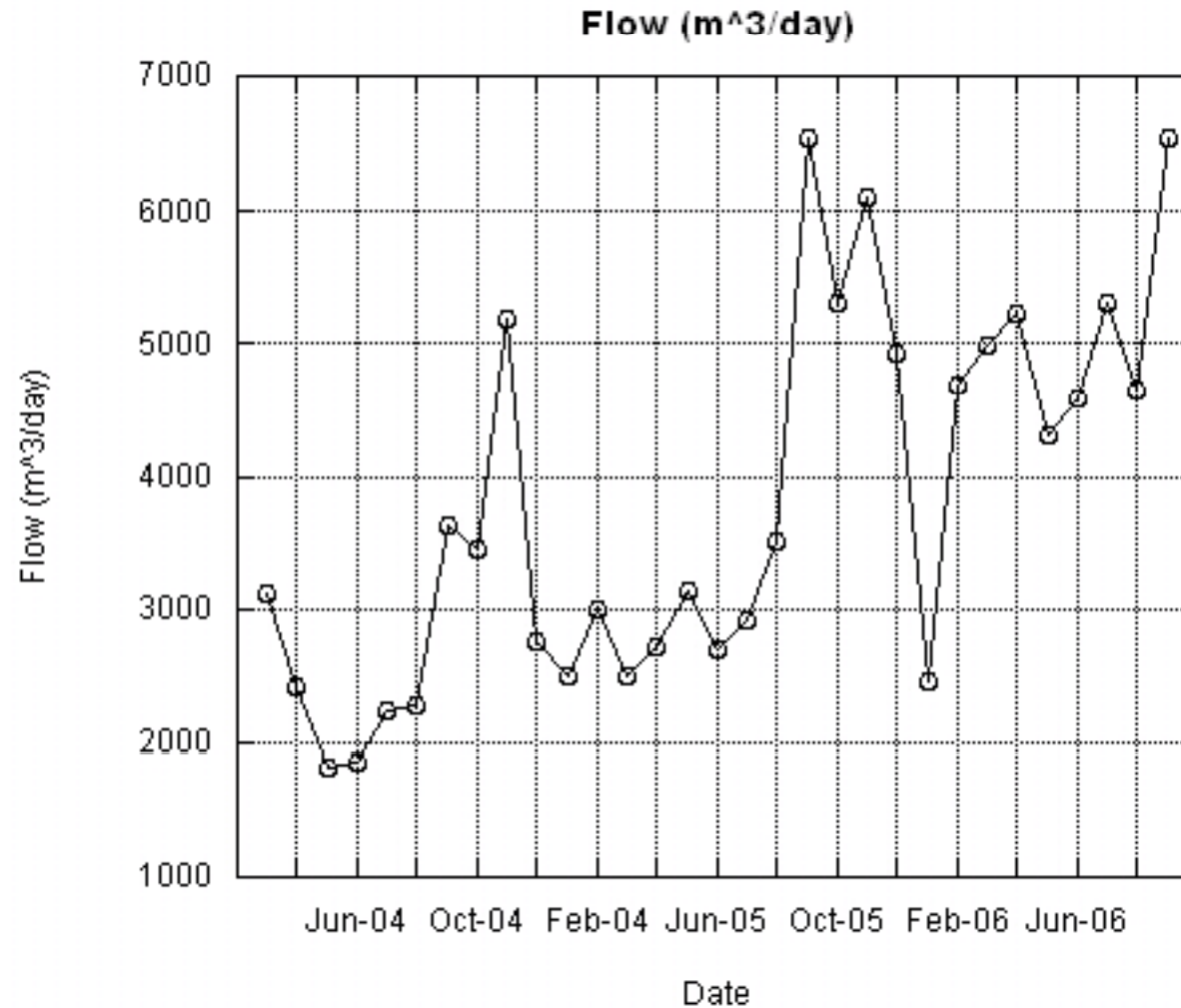
Compound	Wetland Influent	Wetland Effluent
Benzene, mg/L	0.17	Non-detect (0.01)
BTEX, mg/L	0.47	Non-detect (0.01)
GRO, mg/L	2.02	Non-detect (0.05)

Compound	k_A , m/yr	
Benzene	~ 240	
BTEX	~ 350	k_A based on 3 TIS
GRO	~ 325	





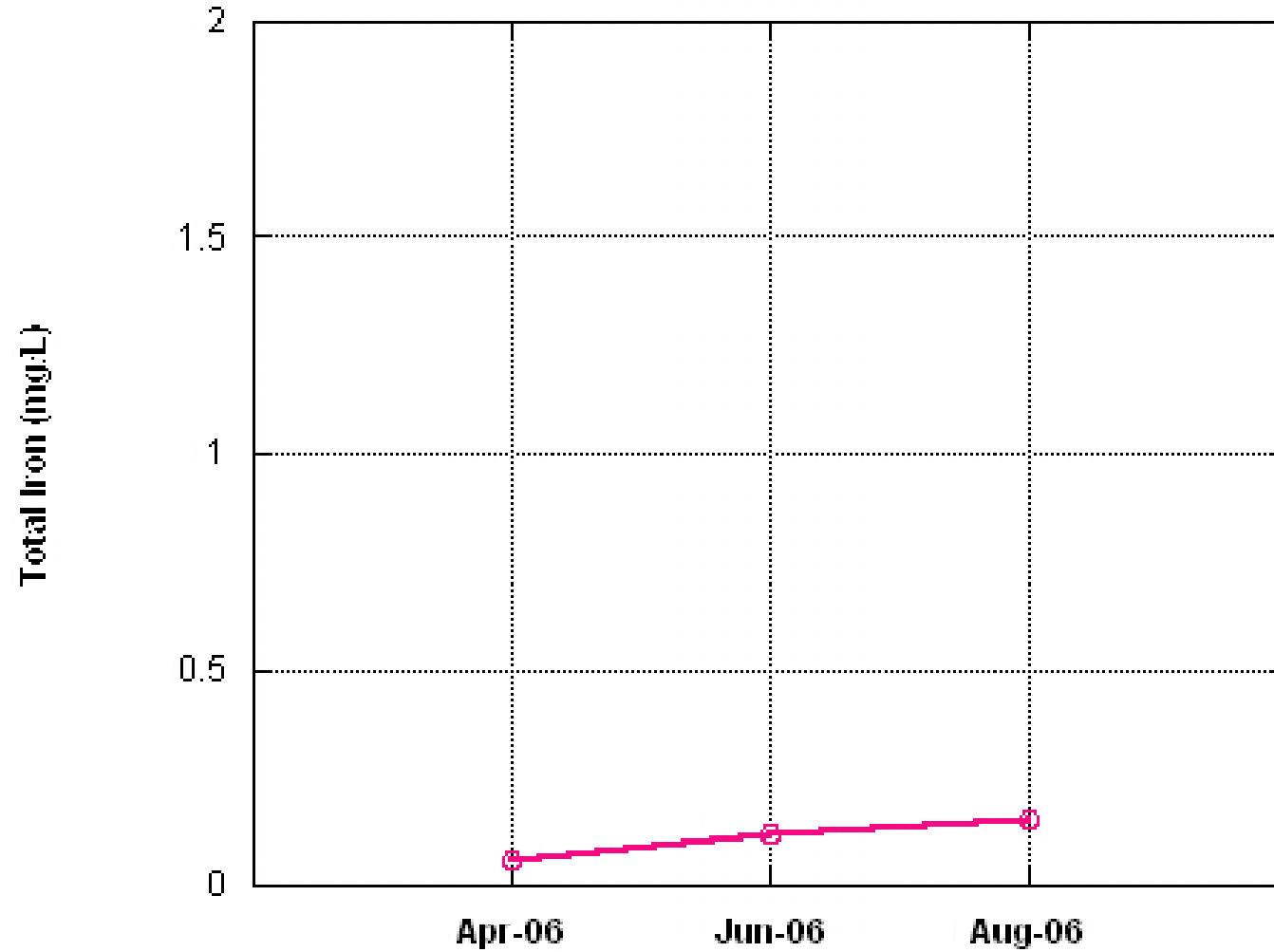
Approaching Design Flow





Effluent Iron Concentrations

2006 SSF Effluent Total Iron Concentration (mg/L)

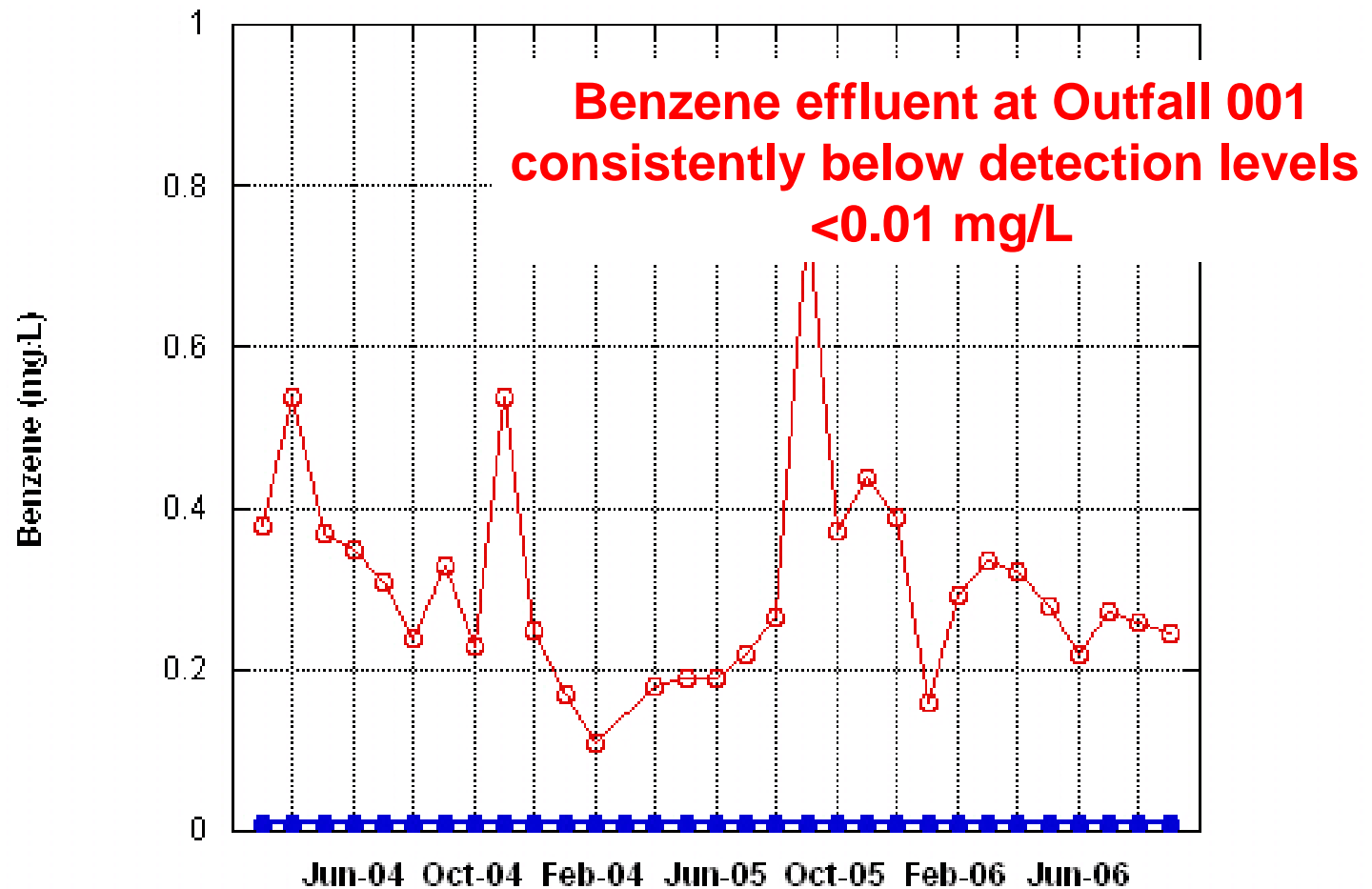




Benzene Data: 2004 - 2006

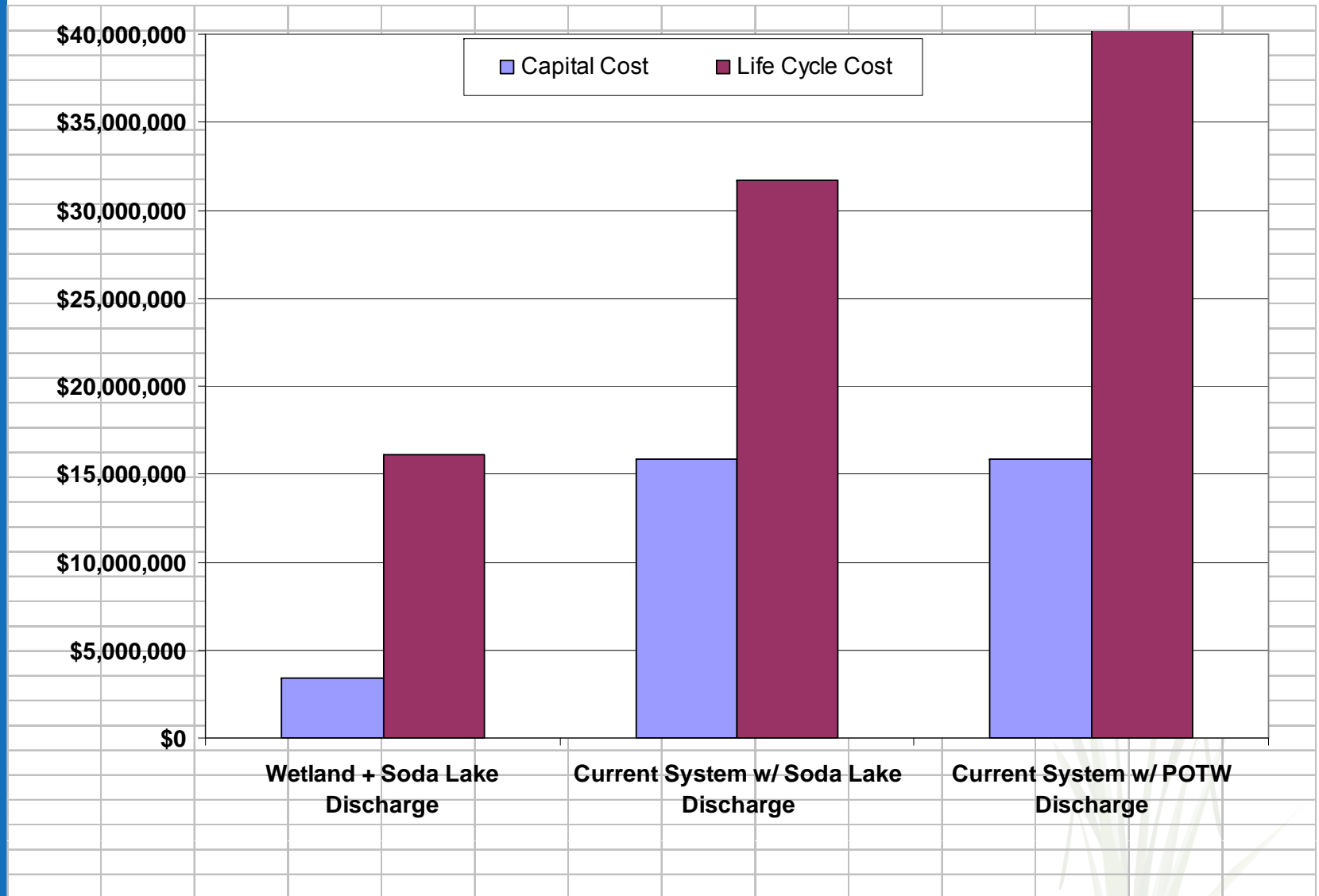


Benzene influent and effluent, entire system





Cost Savings to BP: Significant





Evapotranspiration and Engineered Wetland Design in Arid Climates

- Evapotranspiration (ET) is an important design parameter in arid climates
- The energy balance method can be used to calculate water losses due to ET

Energy Inputs – Energy Outputs = Change in Energy Storage (Δ)

$$[R_N + U_{in} + G] - [\lambda\rho ET \pm E_{loss} + U_{out}] = \Delta$$

(MJ/m²·d)





The Penman Equation

- The Penman Equation is used to calculate ET

$$\lambda ET = \Phi(R_N - G) + (1 - \Phi) \lambda K_e [P_w^{\text{sat}}(T) - P_w^{\text{sat}}(T_{\text{dp}})]$$

λ is the volumetric latent heat of water vaporization

Φ is the “Penman Estimator”

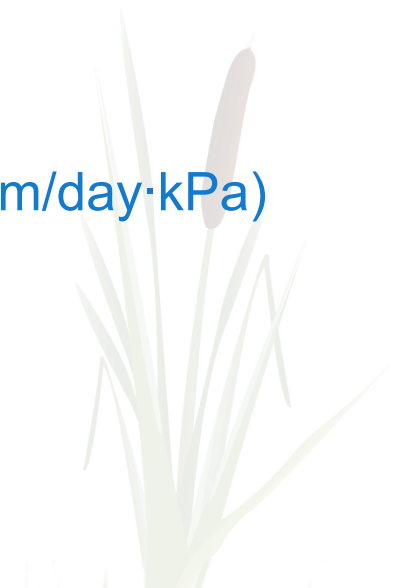
R_N is net solar radiation

G is conductive heat transfer to ground

K_e is the water vapor mass transfer coefficient (m/day·kPa)

P_w^{sat} is saturation water vapor pressure

T is temperature (dp = dew point)

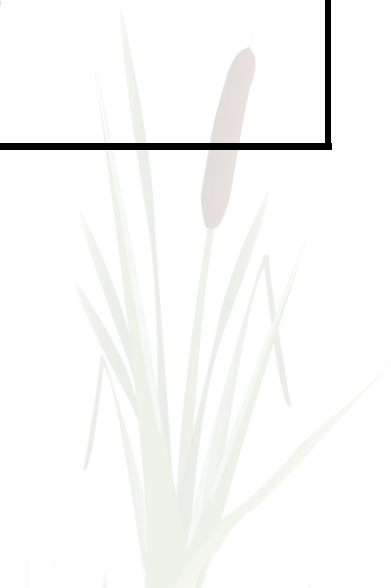




Abu Dhabi design: ET effects

	ET (m/day)	Volume of water lost to ET (m ³ /day)	% of water lost from wetland
Summer	0.0162	19.44	39
Winter	0.0021	2.56	5

Summer: high temperature, low RH
Winter: higher RH





Conclusions

- Aeration + wetland sod improved BTEX removal
- Cascade aerator + FWS wetlands effective in iron removal
- Full-scale system has produced non-detect effluent concentrations since May 2003
- BTEX k_A pilot: 356 m/yr (3 TIS)
- BTEX k_A full scale: 350 m/yr (3 TIS)





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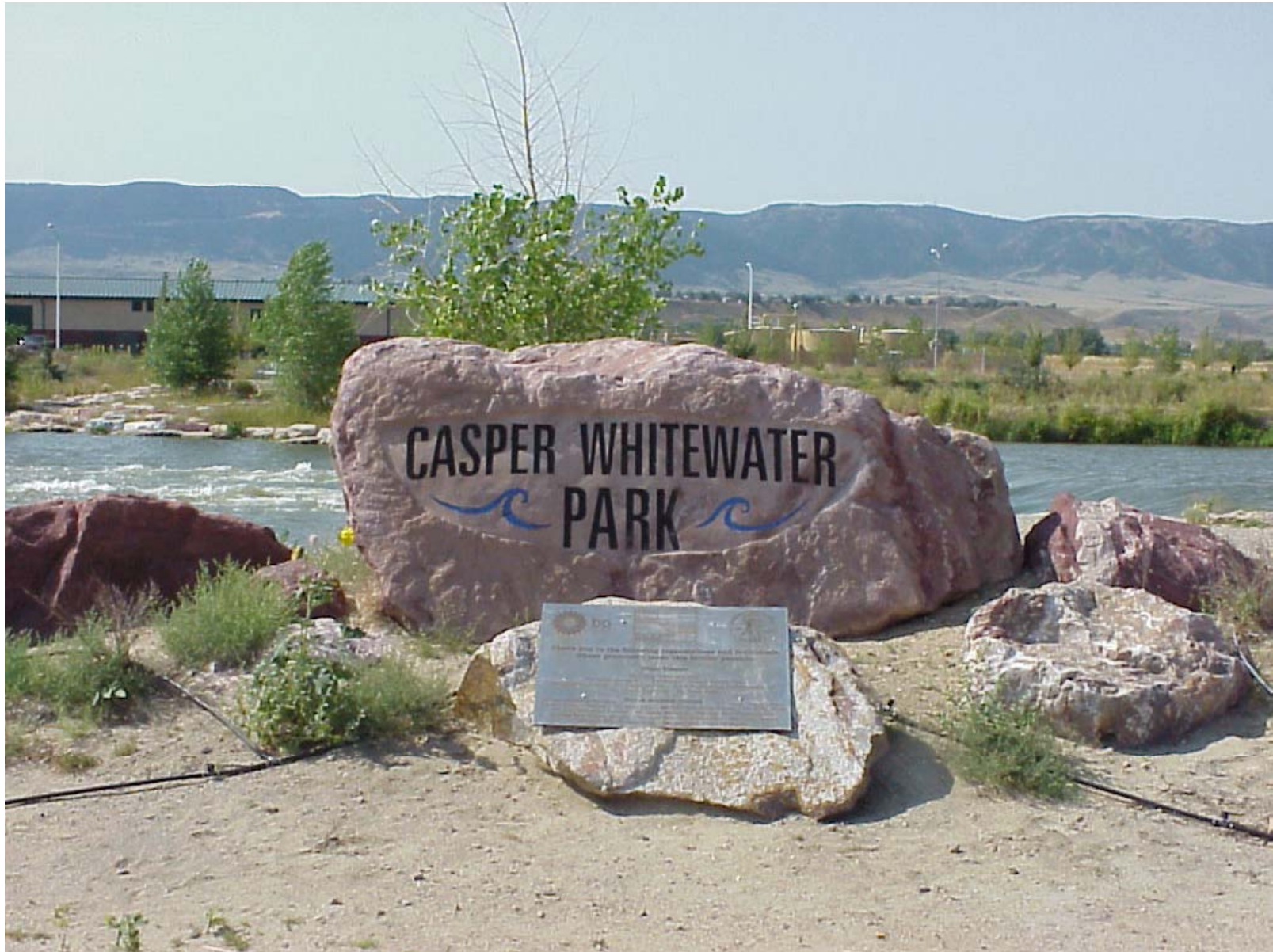


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Questions?

